# Development and Application of Coupled Hurricane Wave and Surge Models for Southern Louisiana

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University of Notre Dame

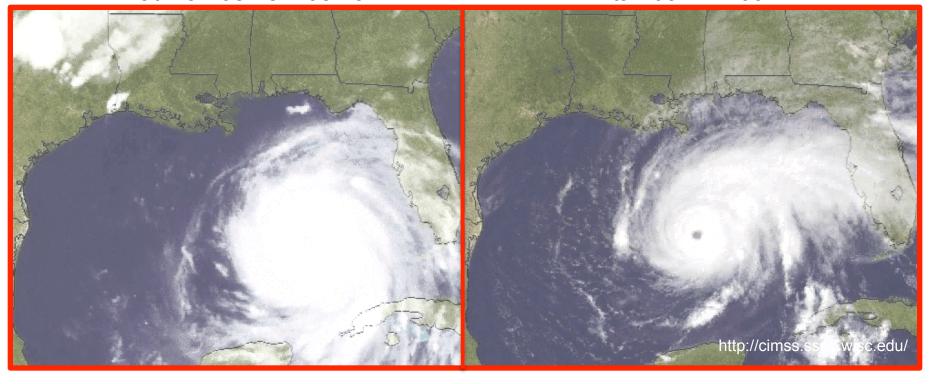
Ocean Engineering Seminar Series, Texas A&M University
Thursday, 10 February 2011



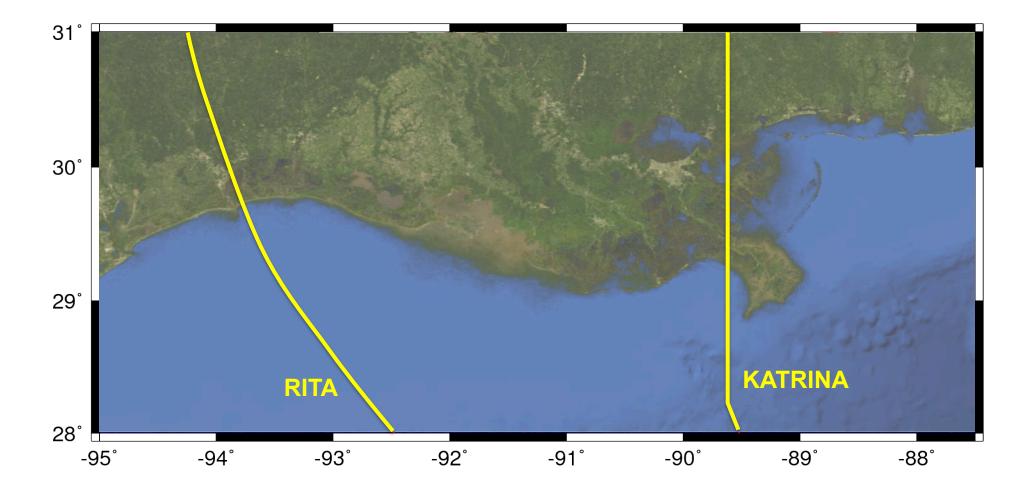
- S. Bunya, *et al.* (2010). "A High-Resolution Coupled Riverine Flow, Tide, Wind, Wind Wave, and Storm Surge Model for Southern Louisiana and Mississippi, Part I: Model Development and Validation." *Monthly Weather Review* 138, 345-377.
- J.C. Dietrich, *et al.* (2010). "A High-Resolution Coupled Riverine Flow, Tide, Wind, Wind Wave, and Storm Surge Model for Southern Louisiana and Mississippi, Part II: Synoptic Description and Analysis of Hurricanes Katrina and Rita." *Monthly Weather Review* 138, 378-404.

#### 2005 Hurricane Season

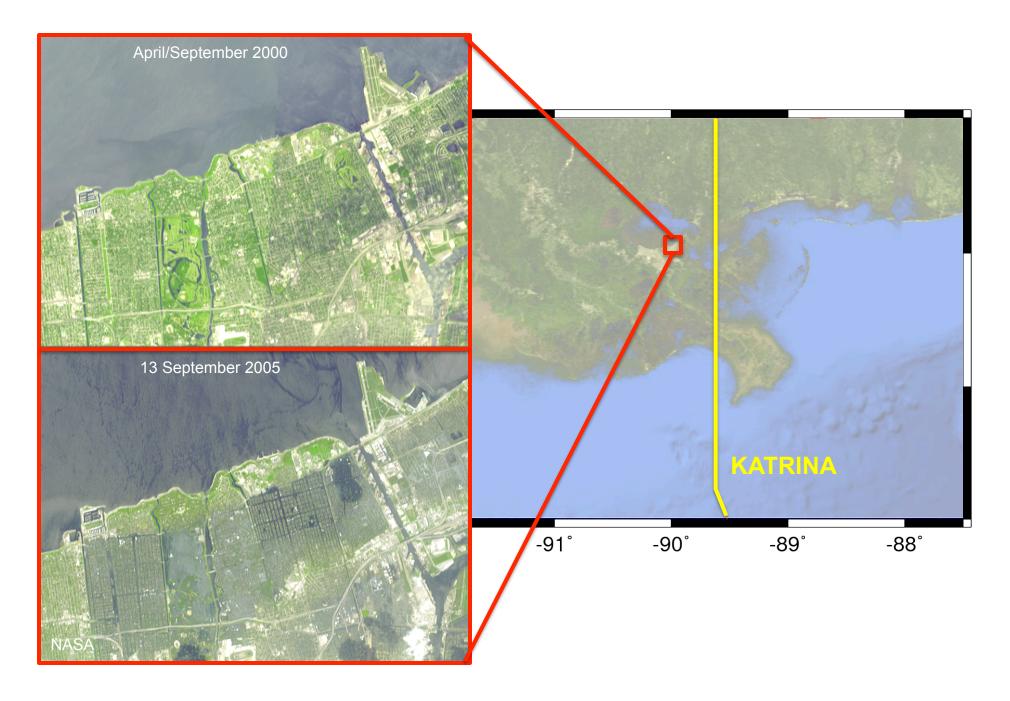
Katrina: 08/28 – 08/29 Rita: 09/22 – 09/24



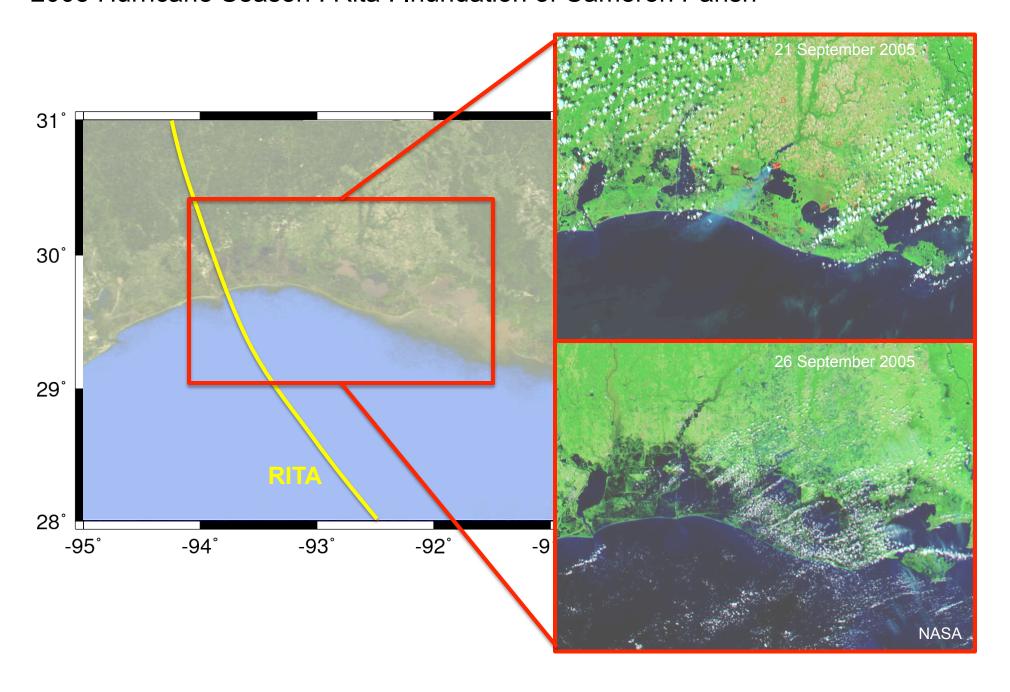
#### 2005 Hurricane Season



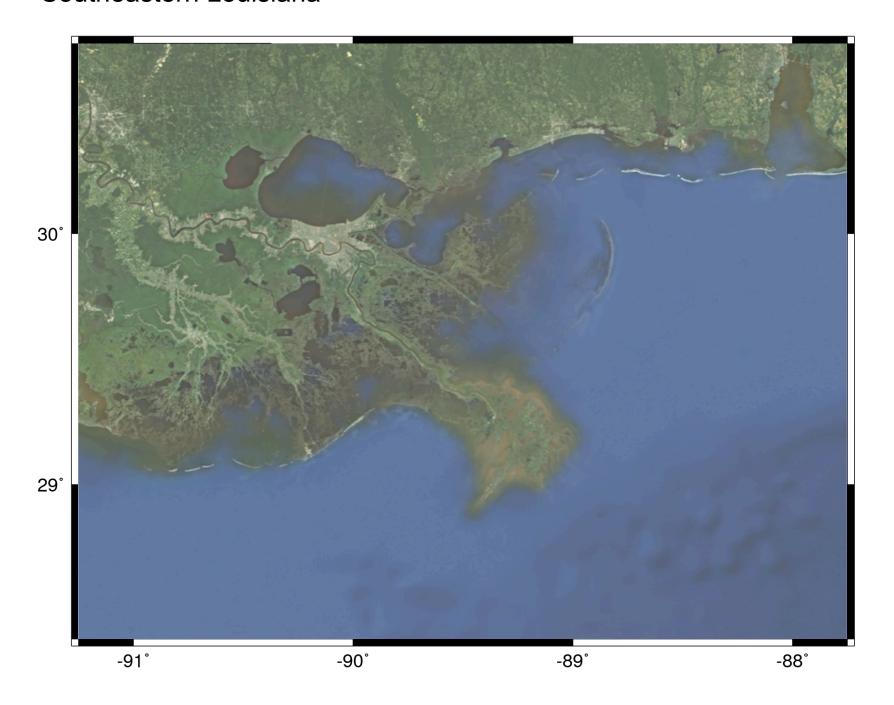
## 2005 Hurricane Season: Katrina: Inundation of New Orleans



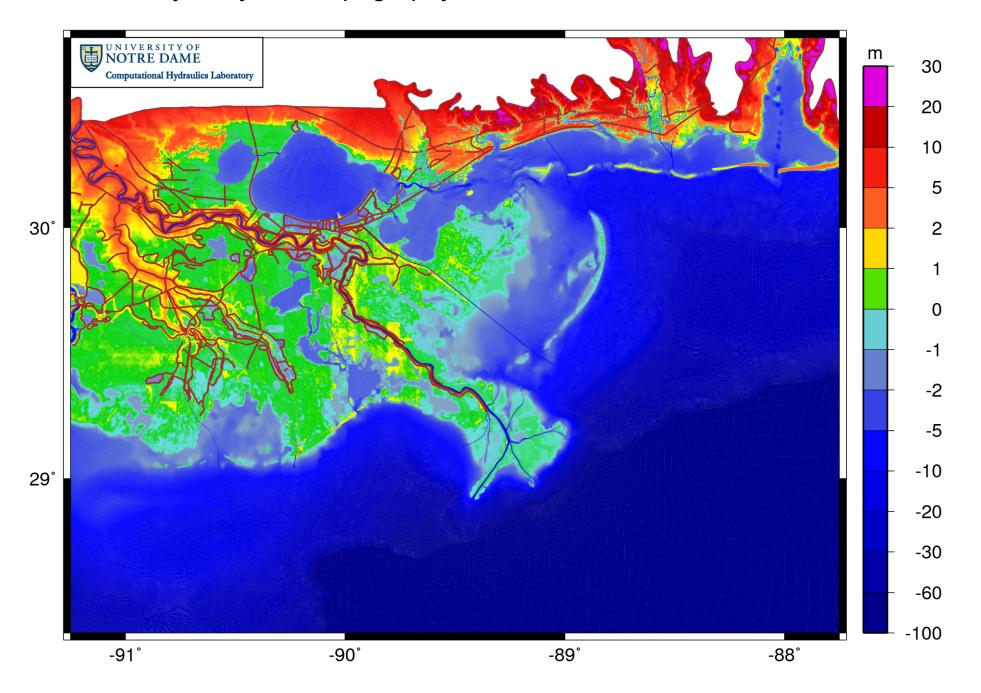
#### 2005 Hurricane Season: Rita: Inundation of Cameron Parish



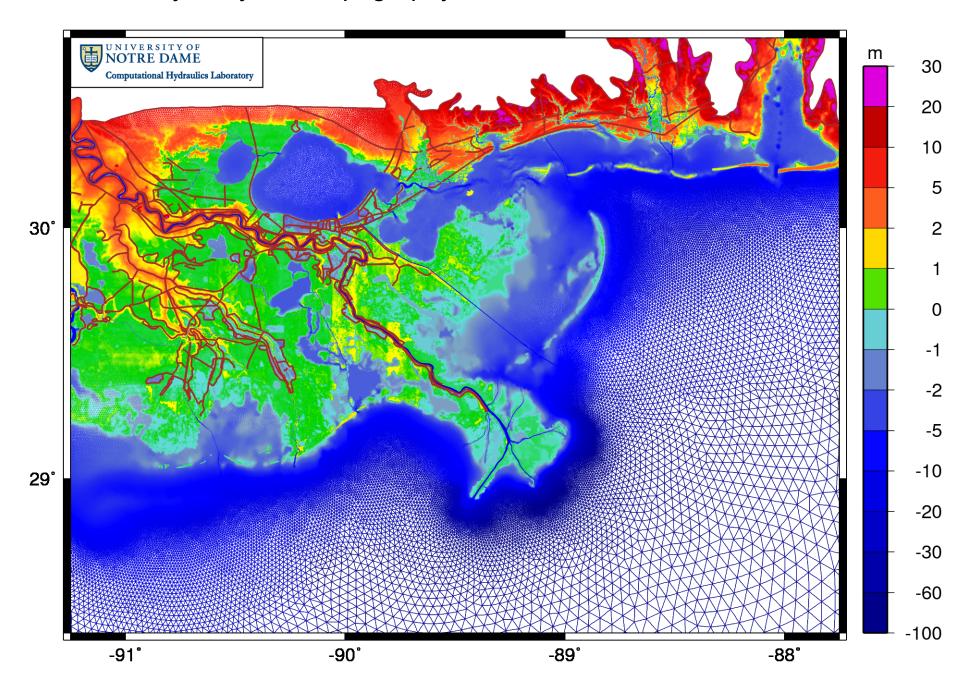
## Southeastern Louisiana



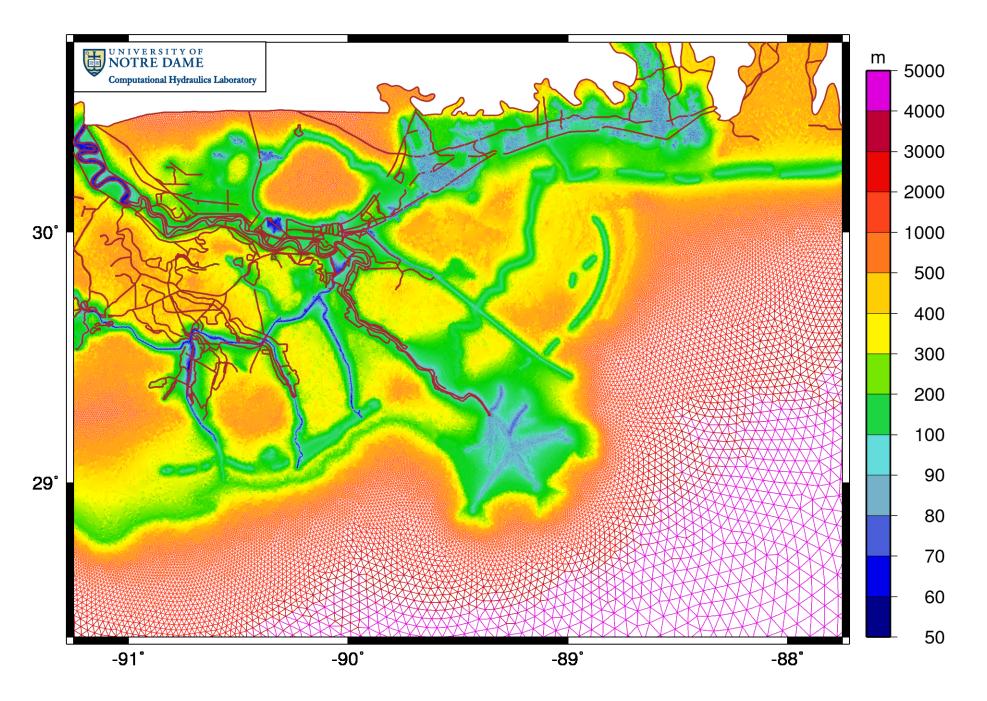
SL15: Bathymetry and Topography



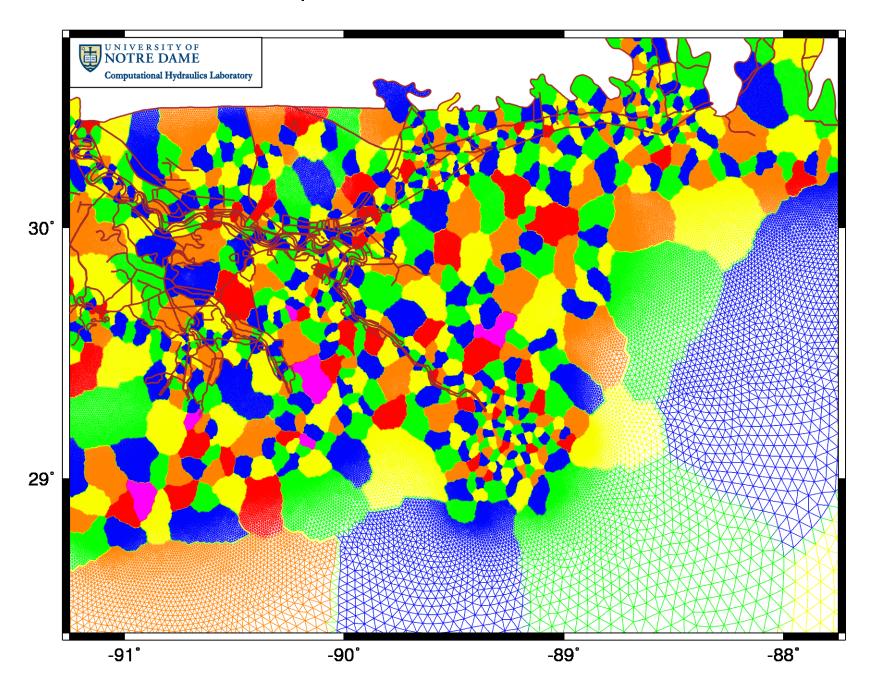
SL15: Bathymetry and Topography



SL15: Mesh Sizes



SL15: Domain Decomposition



#### **ADCIRC**: Governing Equations

#### **ADvanced CIRCulation (ADCIRC):**

Solves the Generalized Wave Continuity Equation (GWCE):

$$\frac{\partial^2 \xi}{\partial t^2} + \tau_0 \frac{\partial \xi}{\partial t} + \frac{\partial \tilde{J}_x}{\partial x} + \frac{\partial \tilde{J}_y}{\partial y} - UH \frac{\partial \tau_0}{\partial x} - VH \frac{\partial \tau_0}{\partial y} = 0$$

· where:

$$\tilde{J}_{x} = -Q_{x} \frac{\partial U}{\partial x} - Q_{y} \frac{\partial U}{\partial y} + fQ_{y} - \frac{g}{2} \frac{\partial \zeta^{2}}{\partial x} - gH \frac{\partial}{\partial x} \left[ \frac{p_{s}}{g\rho_{0}} - \alpha \eta \right] + \frac{\tau_{sx} + \tau_{bx}}{\rho_{0}} + \left( M_{x} - D_{x} \right) + U \frac{\partial \zeta}{\partial t} + \tau_{0} Q_{x} - gH \frac{\partial \zeta}{\partial x}$$

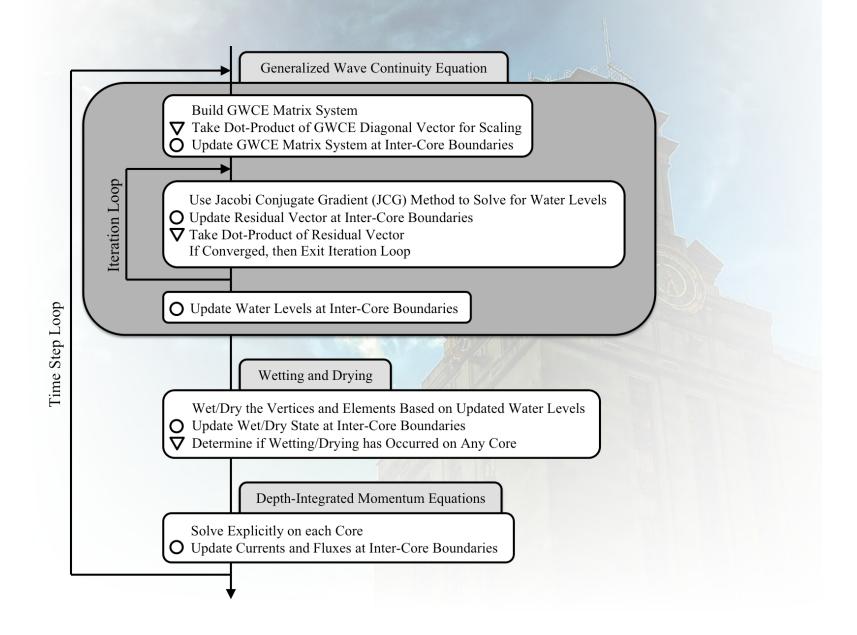
$$\tilde{J}_{y} = -Q_{x} \frac{\partial V}{\partial x} - Q_{y} \frac{\partial V}{\partial y} - fQ_{x} - \frac{g}{2} \frac{\partial \zeta^{2}}{\partial y} - gH \frac{\partial}{\partial y} \left[ \frac{p_{s}}{g\rho_{0}} - \alpha \eta \right] + \frac{\tau_{sy} + \tau_{by}}{\rho_{0}} + \left( M_{y} - D_{y} \right) + V \frac{\partial \zeta}{\partial t} + \tau_{0}Q_{y} - gH \frac{\partial \zeta}{\partial y}$$

Solves the vertically-integrated momentum equations:

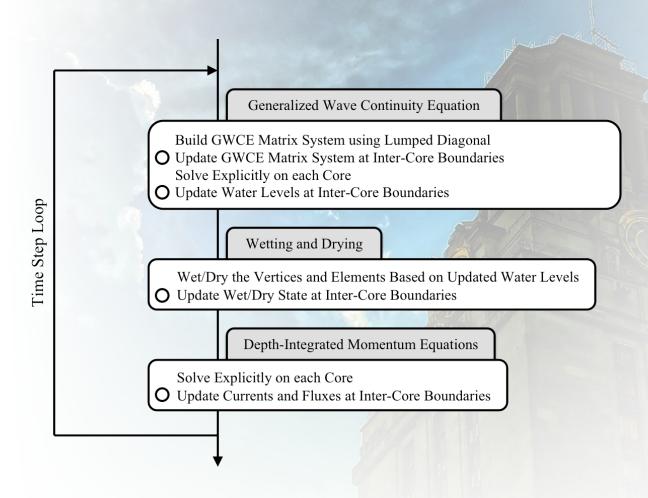
$$\frac{\partial U}{\partial t} + U \frac{\partial U}{\partial x} + V \frac{\partial U}{\partial y} - fV = -g \frac{\partial}{\partial x} \left[ \zeta + \frac{p_s}{g \rho_0} - \alpha \eta \right] + \frac{\tau_{sx} + \tau_{bx}}{\rho_0 H} + \frac{M_x - D_x}{H}$$

$$\frac{\partial V}{\partial t} + U \frac{\partial V}{\partial x} + V \frac{\partial V}{\partial y} + fU = -g \frac{\partial}{\partial y} \left[ \zeta + \frac{p_s}{g \rho_0} - \alpha \eta \right] + \frac{\tau_{sy} + \tau_{by}}{\rho_0 H} + \frac{M_y - D_y}{H}$$

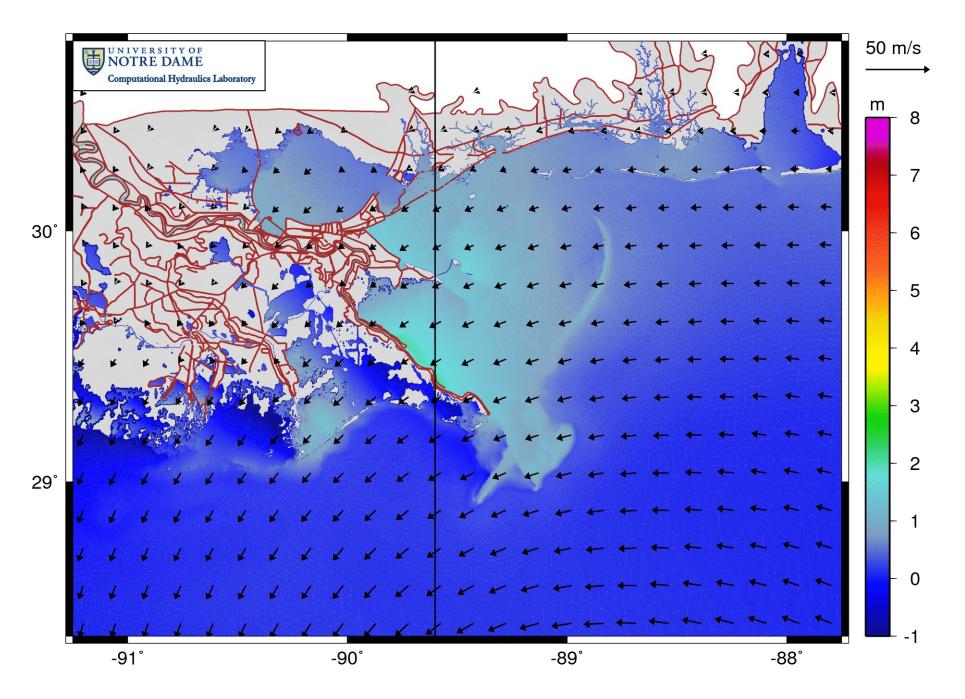
#### ADCIRC: Flowchart: Implicit Solution of GWCE



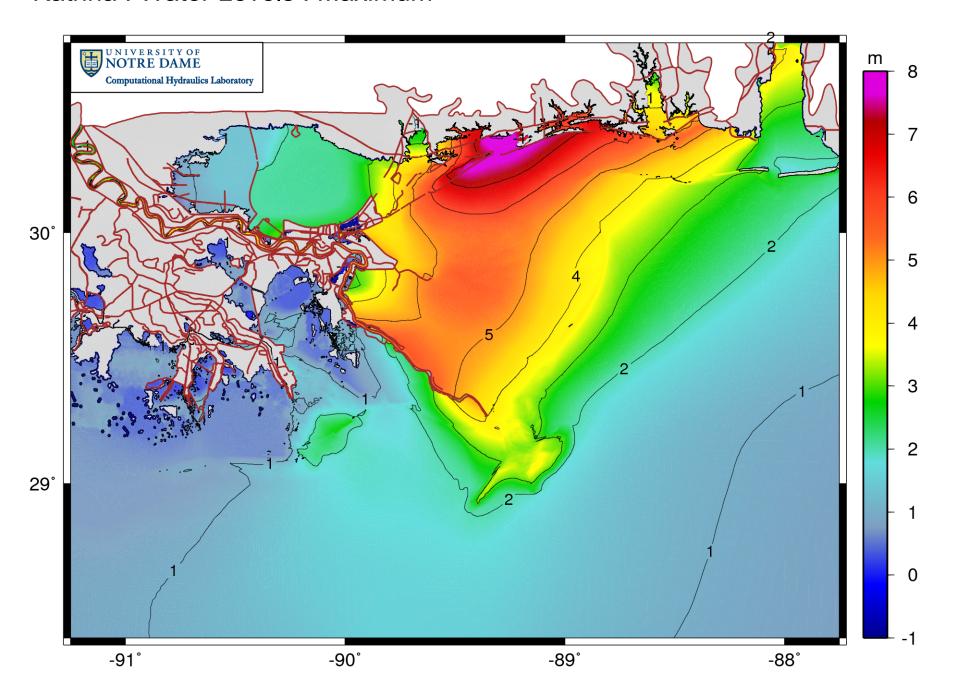
#### ADCIRC: Flowchart: Explicit Solution of GWCE



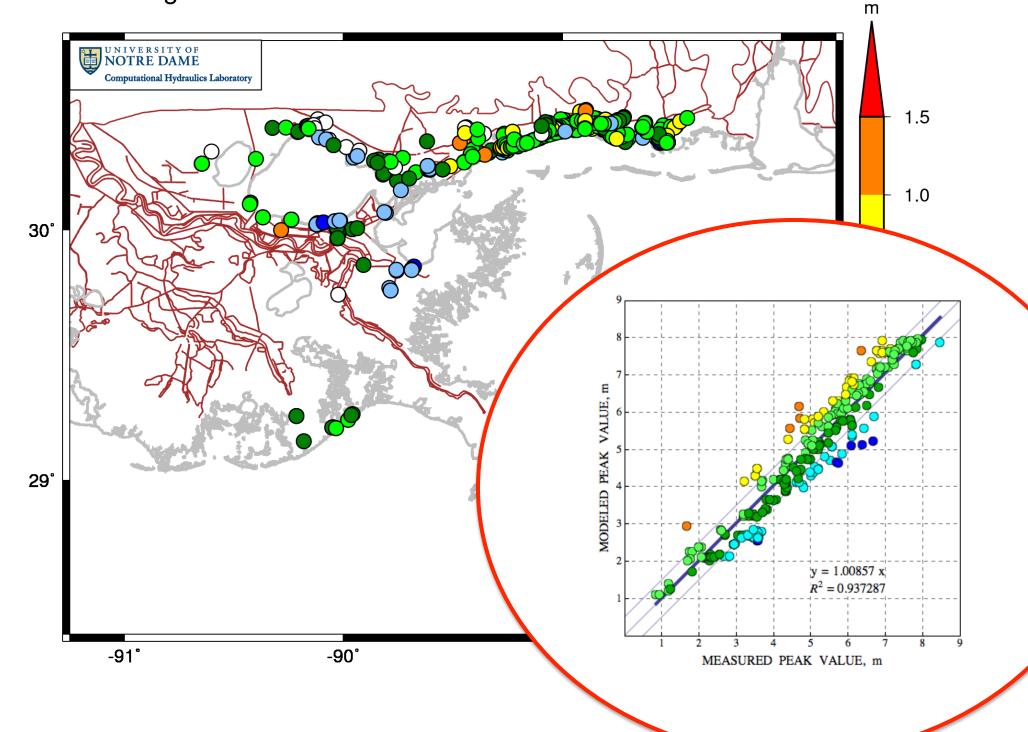
#### Katrina: Water Levels: 2005/08/29



#### Katrina: Water Levels: Maximum



## Katrina: High-Water Marks



#### 'Loose' Coupling to STWAVE

#### **STeady-state WAVE (STWAVE):**

- Propagates wave action density N(t, x, y, σ, θ)
- Developed by USACE

#### **Passing of Radiation Stress Gradients:**

Integrate action density to get radiation stresses:

$$S_{xx} = \rho_0 g \iint \left( n \cos^2 \theta + n - \frac{1}{2} \right) \sigma N d\sigma d\theta$$

$$S_{xy} = \rho_0 g \iint (n \sin \theta \cos \theta) \sigma N d\sigma d\theta$$

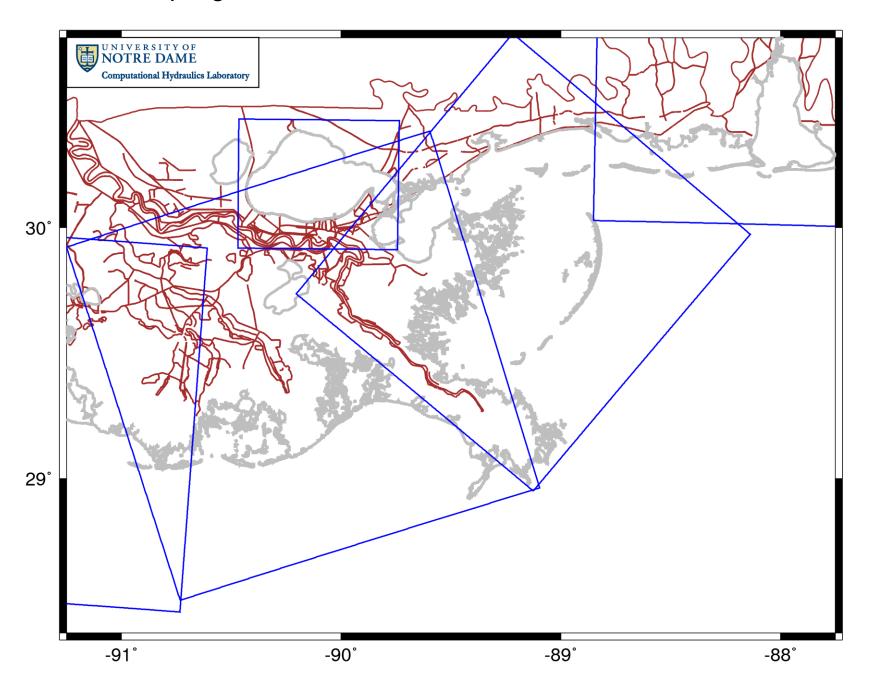
$$S_{yy} = \rho_0 g \iint \left( n \sin^2 \theta + n - \frac{1}{2} \right) \sigma N d\sigma d\theta$$

Pass the gradients as surface stresses to ADCIRC:

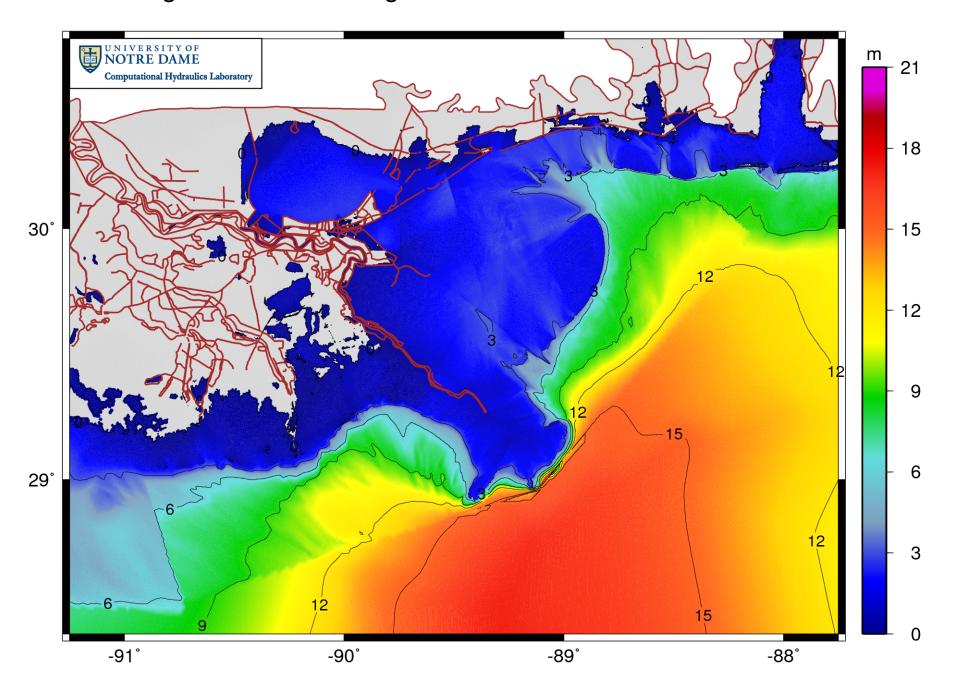
$$\tau_{sx,waves} = -\frac{\partial S_{xx}}{\partial x} - \frac{\partial S_{xy}}{\partial y}$$

$$\tau_{sy,waves} = -\frac{\partial S_{xy}}{\partial x} - \frac{\partial S_{yy}}{\partial y}$$

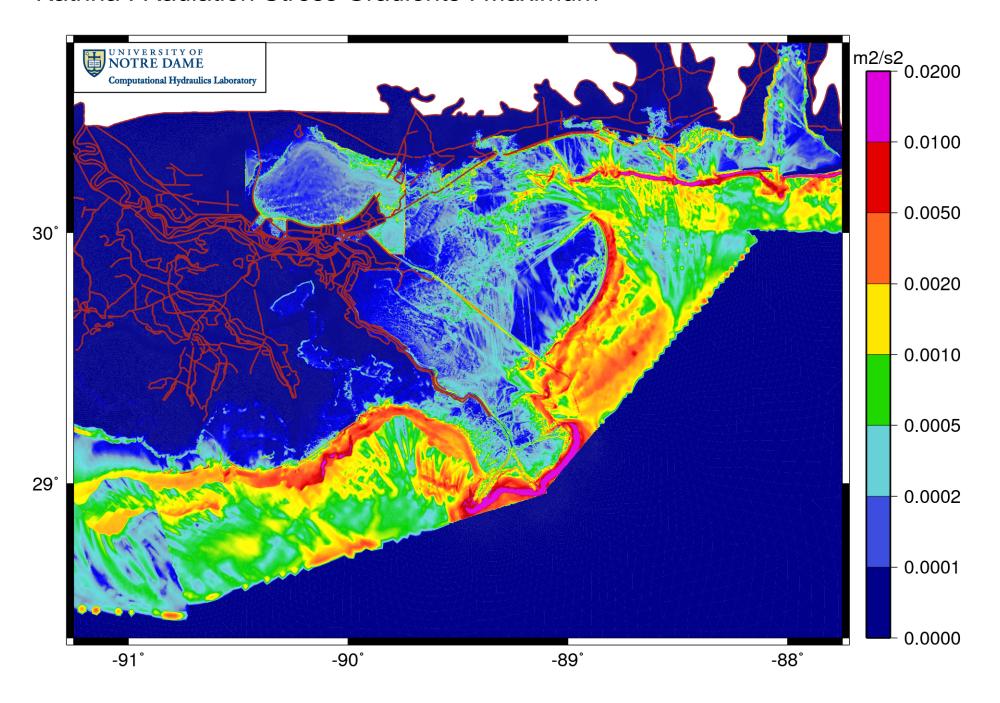
## 'Loose' Coupling to STWAVE



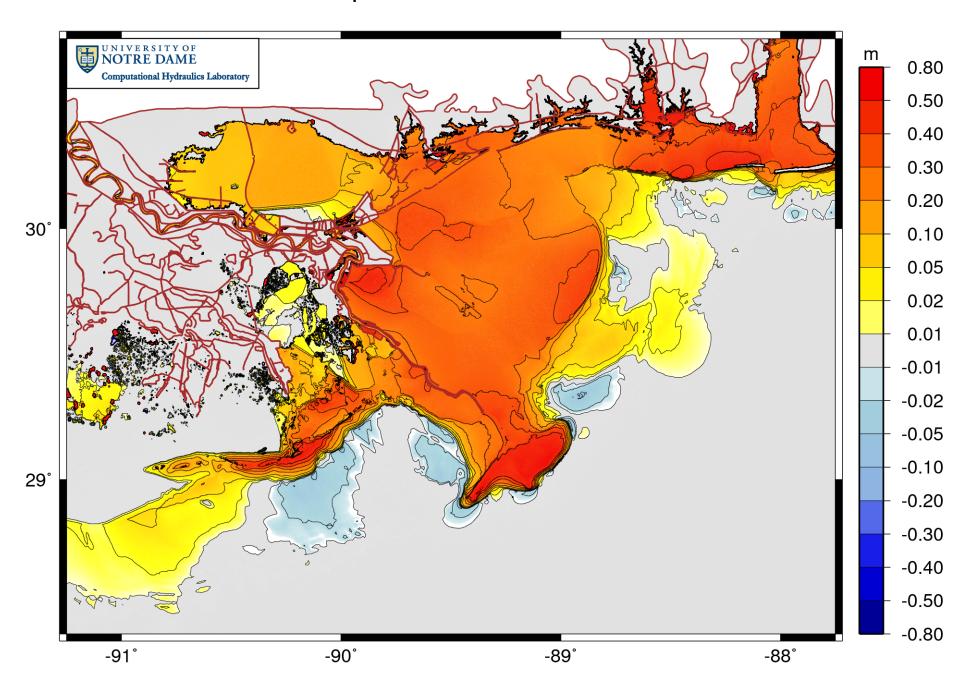
## Katrina: Significant Wave Heights: Maximum



#### Katrina: Radiation Stress Gradients: Maximum



#### Katrina: Wave-Driven Setup: Maximum

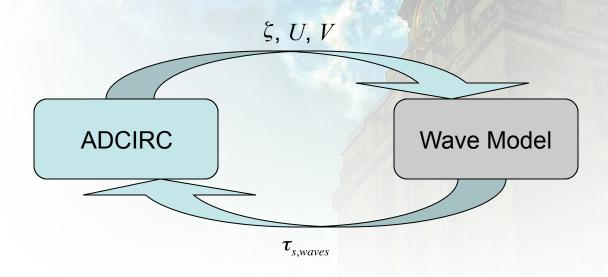




- J.C. Dietrich, *et al.* (2011). "Modeling Hurricane Waves and Storm Surge using Integrally-Coupled, Scalable Computations." *Coastal Engineering*, 58, 45-65.
- J.C. Dietrich, et al. (2011). "Performance of the Unstructured-Mesh, SWAN+ADCIRC Model in Computing Hurricane Waves and Surge." Journal of Scientific Computing, in preparation.

#### Disadvantages of 'Loose' Coupling

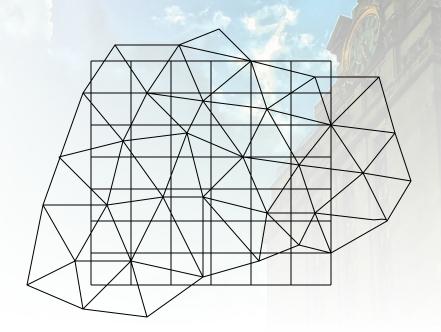
- 1. Interpolation at Wave Model Boundaries
- 2. Coverage in Deep Water
- 3. Iteration
  - Models coupled through input files
    - Winds, water levels and currents passed to wave model
    - Radiation stress gradients passed to ADCIRC
  - Process can be automated, but is still inefficient



### Disadvantages of 'Loose' Coupling

#### 4. Interpolation:

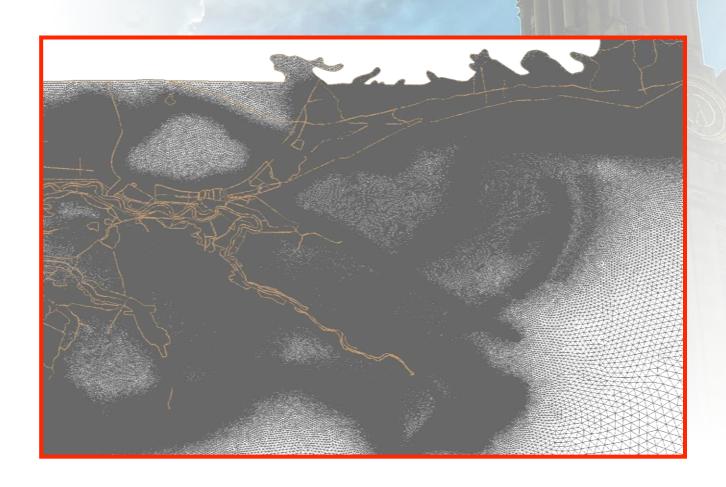
- Wave and circulation models run on different grids
  - Wave models on structured meshes
  - ADCIRC on unstructured, finite element mesh
- Results must be interpolated onto each mesh



## Disadvantages of 'Loose' Coupling

## 5. Resolution in wave breaking zones:

- Circulation model has no knowledge of wave breaking
- Must over-resolve these zones



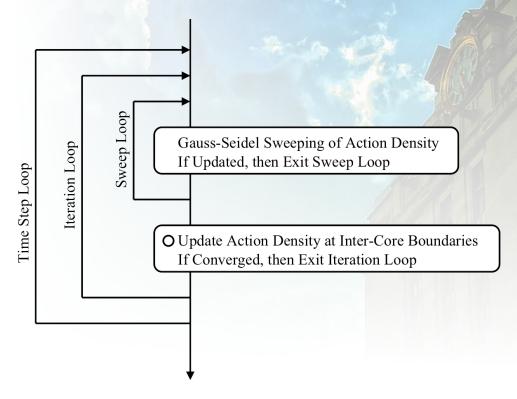
### 'Tight' Coupling of SWAN+ADCIRC

#### Simulating WAves Nearshore (SWAN):

Solves the action balance equation:

$$\frac{\partial N}{\partial t} + \nabla_{\vec{x}} \cdot \left[ \left( \vec{c}_g + \vec{U} \right) N \right] + \frac{\partial c_{\theta} N}{\partial \theta} + \frac{\partial c_{\sigma} N}{\partial \sigma} = \frac{S_{tot}}{\sigma}$$

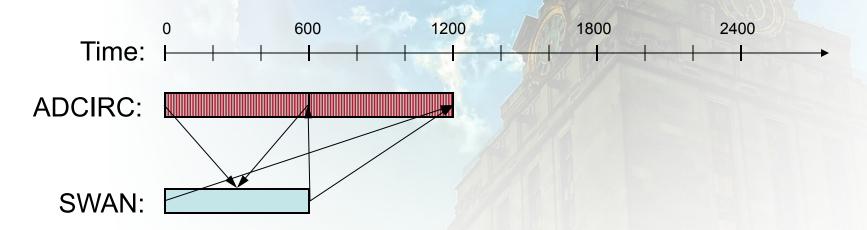
Sweep the action densities throughout the domain:



#### 'Tight' Coupling of SWAN+ADCIRC

#### **Schematic of Coupling:**

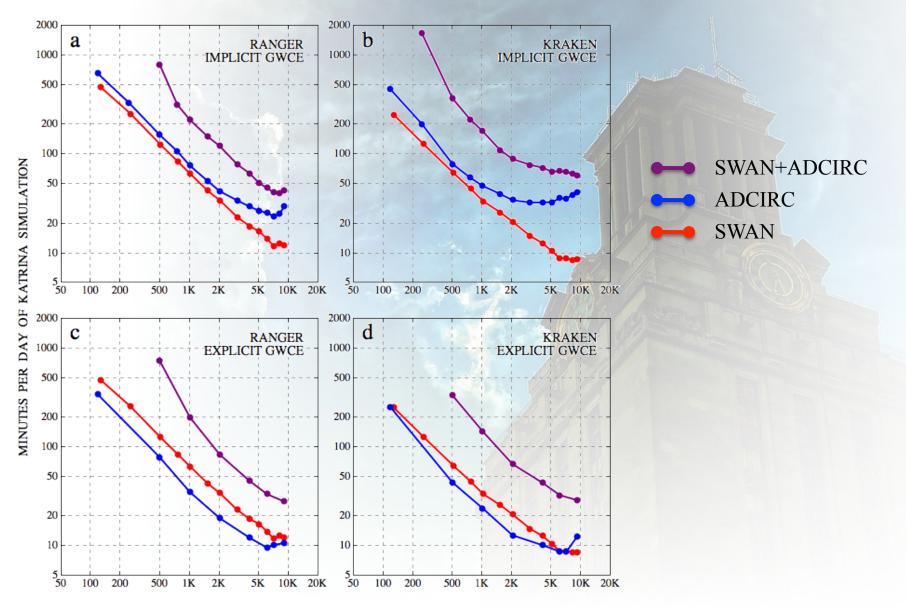
- ADCIRC is run for 600 seconds ( $\Delta t = 1 \text{ sec}$ )
- Water levels (ζ) and currents (U, V) are passed to SWAN
- SWAN is run for 600 seconds ( $\Delta t = 600 \text{ sec}$ )
- Radiation stresses (S) and their gradients ( $\tau_{s,waves}$ ) are computed; gradients are passed to ADCIRC
- Repeat



SWAN and ADCIRC are always extrapolating in time

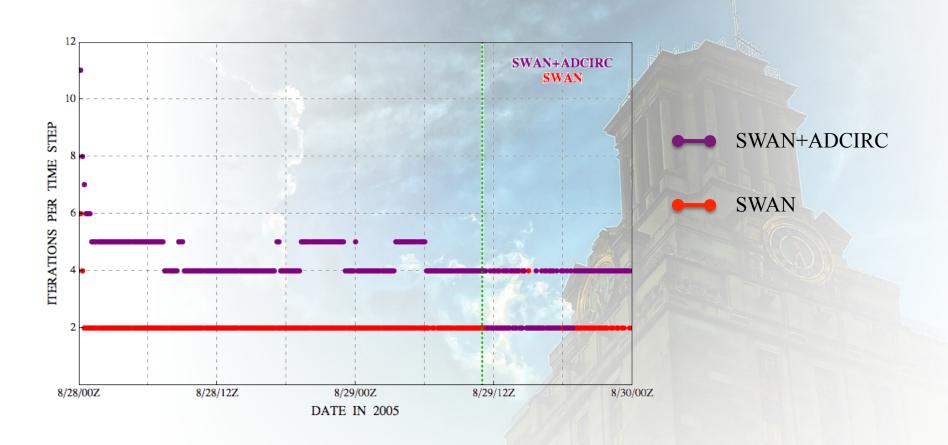
## 'Tight' Coupling of SWAN+ADCIRC **NEIGHBOR CORE** LOCAL CORE SWAN INTER-MODEL INTRA-CORE ADCIRC

## 'Tight' Coupling of SWAN+ADCIRC

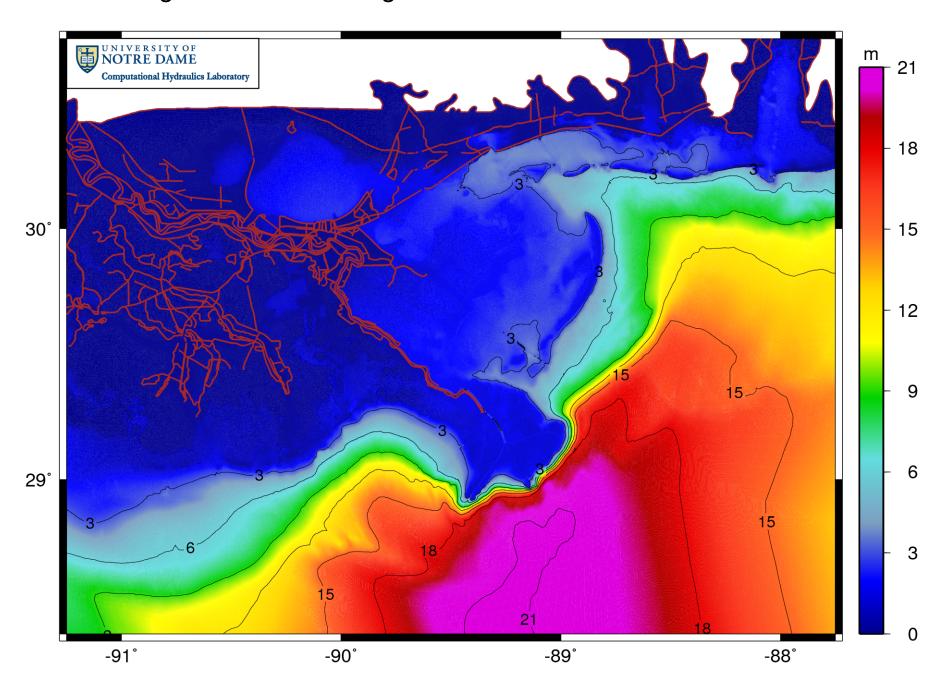


NUMBER OF COMPUTATIONAL CORES

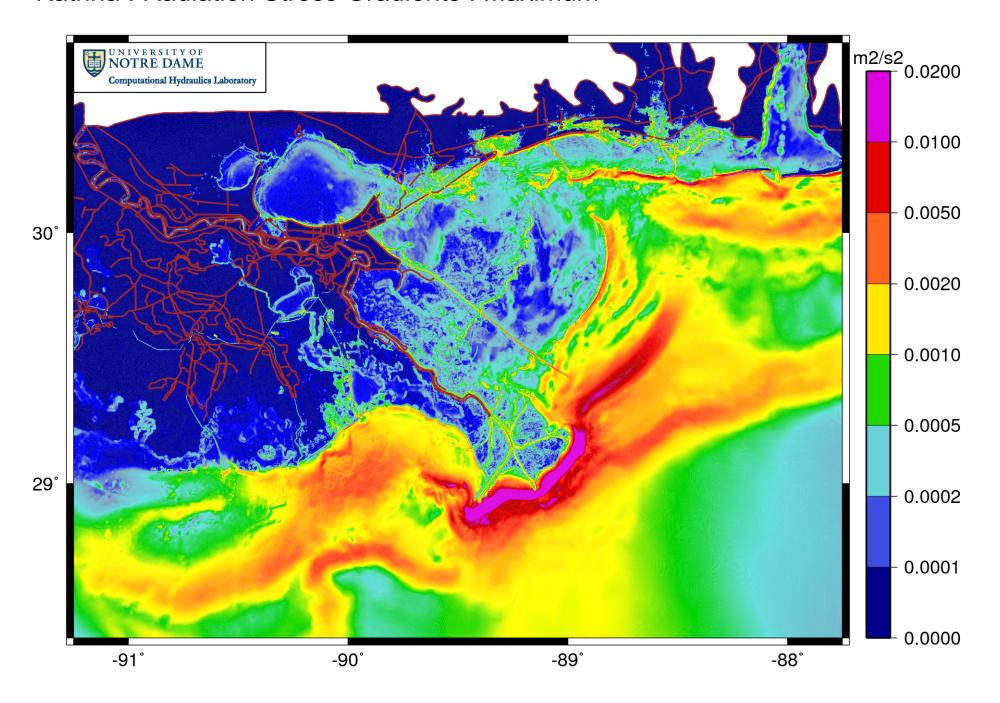
## 'Tight' Coupling of SWAN+ADCIRC



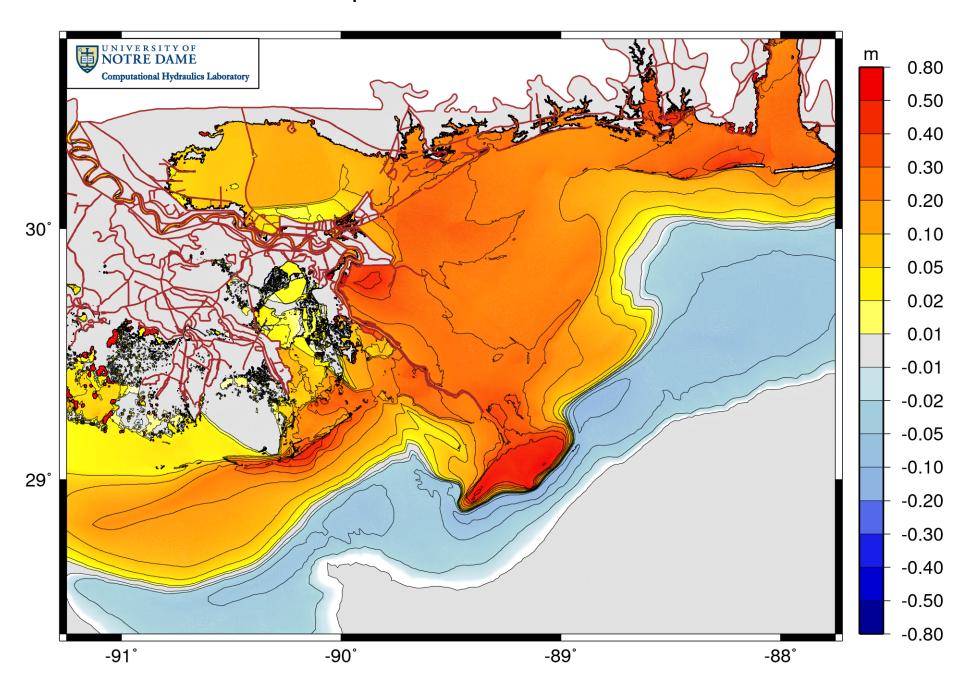
## Katrina: Significant Wave Heights: Maximum

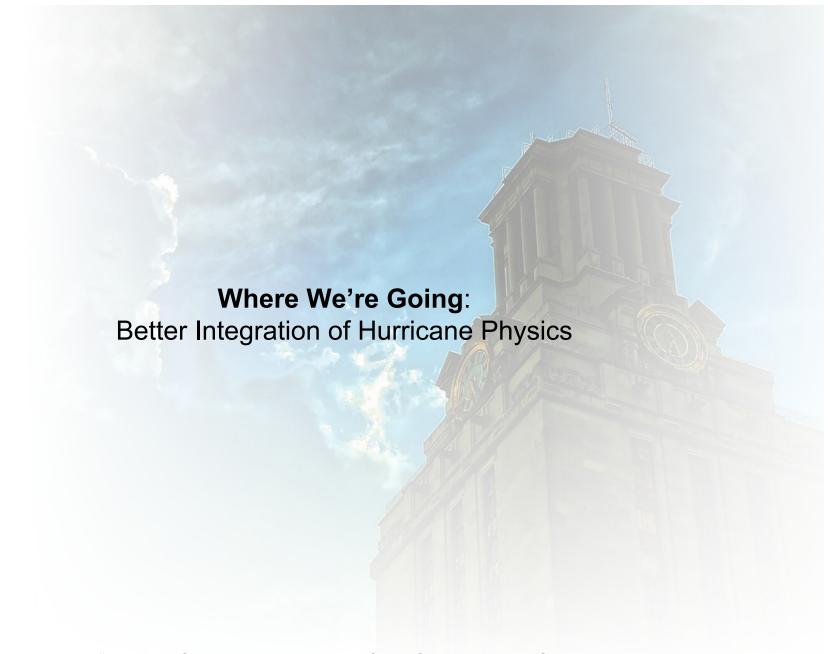


#### Katrina: Radiation Stress Gradients: Maximum



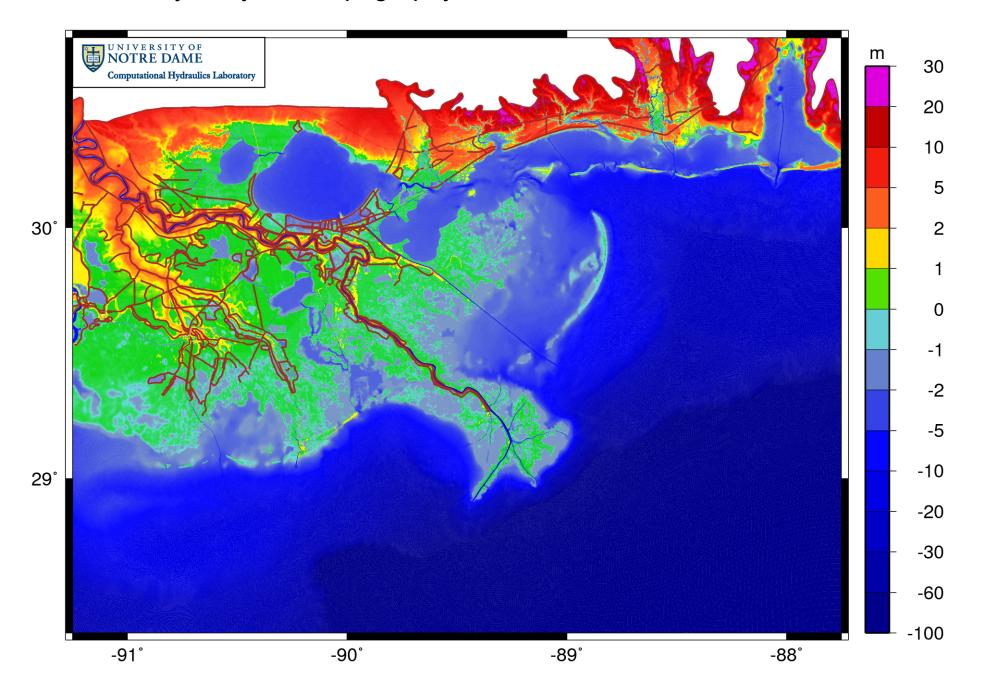
#### Katrina: Wave-Driven Setup: Maximum



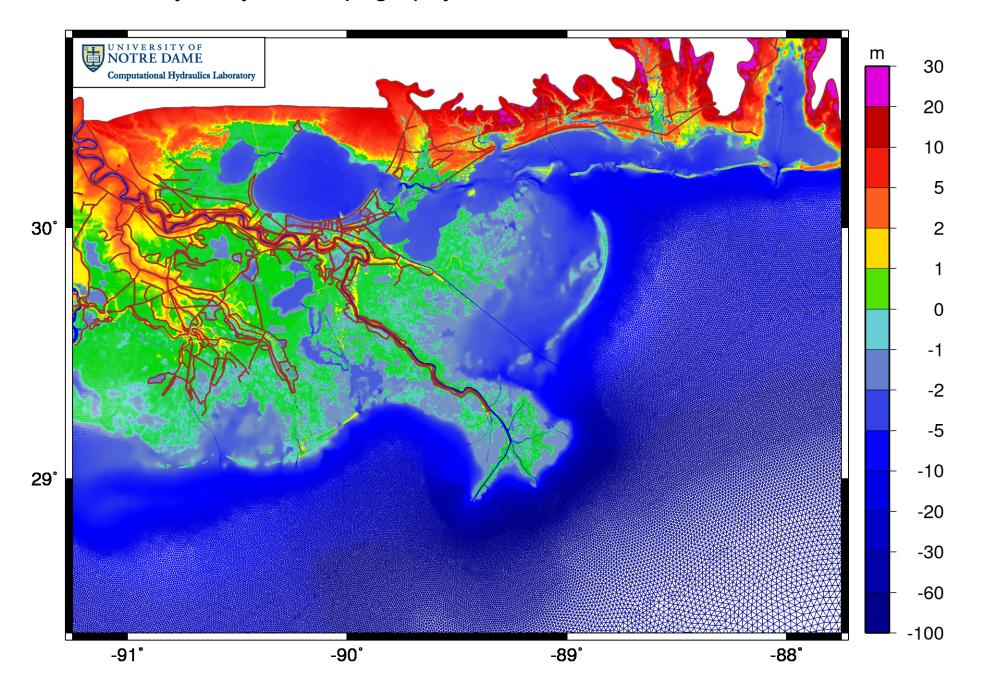


J.C. Dietrich, *et al.* (2011). "Hurricane Gustav (2008) Waves and Storm Surge: Hindcast, Synoptic Analysis and Validation in Southern Louisiana." *Monthly Weather Review*, accepted pending revisions.

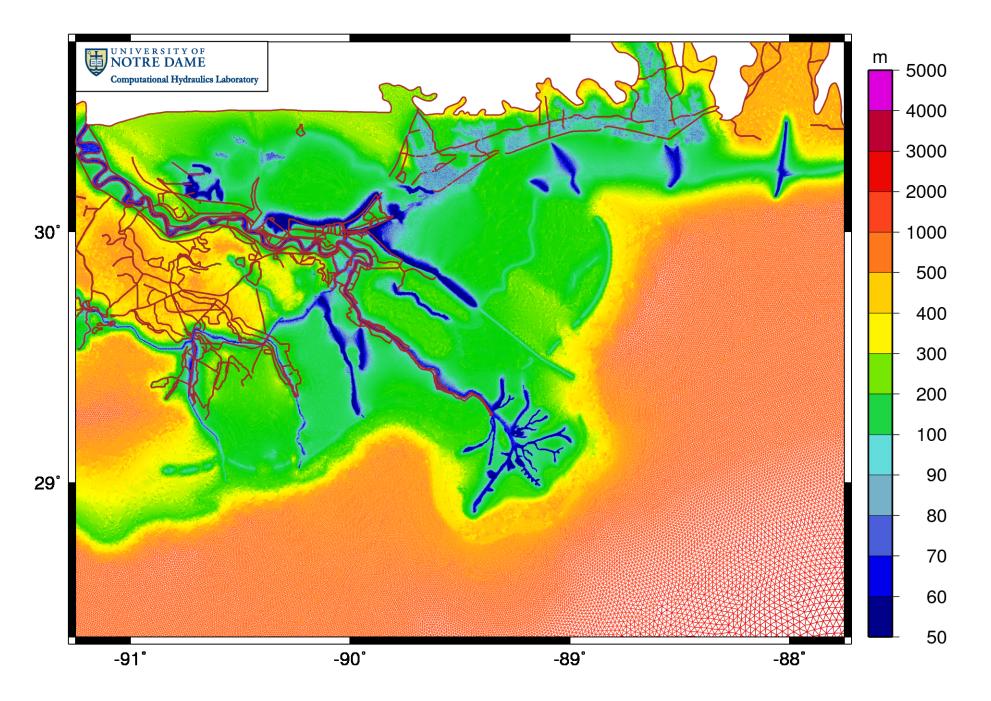
SL16: Bathymetry and Topography

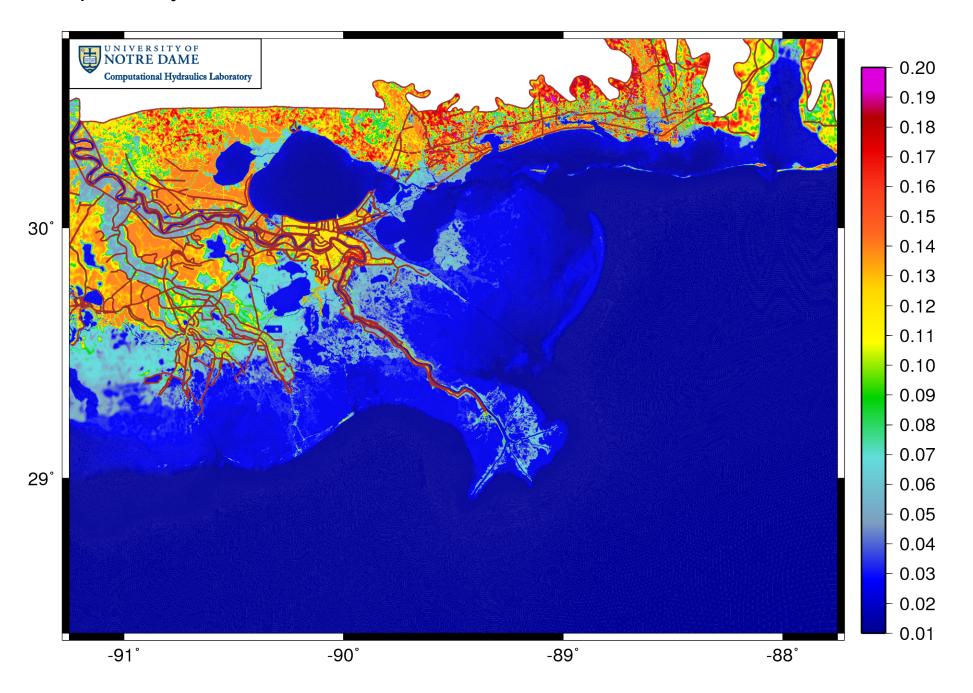


SL16: Bathymetry and Topography



SL16: Mesh Sizes





## **Integrated Coupling of Bottom Friction:**

ADCIRC converts its Manning's n values to bottom stresses:

$$\tau_b = \rho_0 \frac{gn^2}{H^{1/3}} \frac{Q}{H}$$

In SWAN, bottom friction is a dissipation term:

$$S_{ds,b}(\sigma,\theta) = -C_b \frac{\sigma^2}{g^2 \sinh^2 kH} N(\sigma,\theta)$$

where  $C_b$  is a bottom friction coefficient that can be formulated as:

$$C_b = f_w \frac{g}{\sqrt{2}} U_{rms}$$

where  $f_w$  depends on the bottom roughness length scale,  $K_N$ .

We can relate the friction lengths to our Manning's n values:

$$K_N = H \exp\left[-\left(1 + \frac{\kappa H^{1/6}}{n\sqrt{g}}\right)\right]$$

Now we can pass spatially-variable friction lengths to SWAN!

## Wind Drag based on Storm Sectors:

SWAN+ADCIRC applies a sea-surface momentum stress:

$$\tau_{s,winds} = \rho_0 C_d U_{10}^2$$

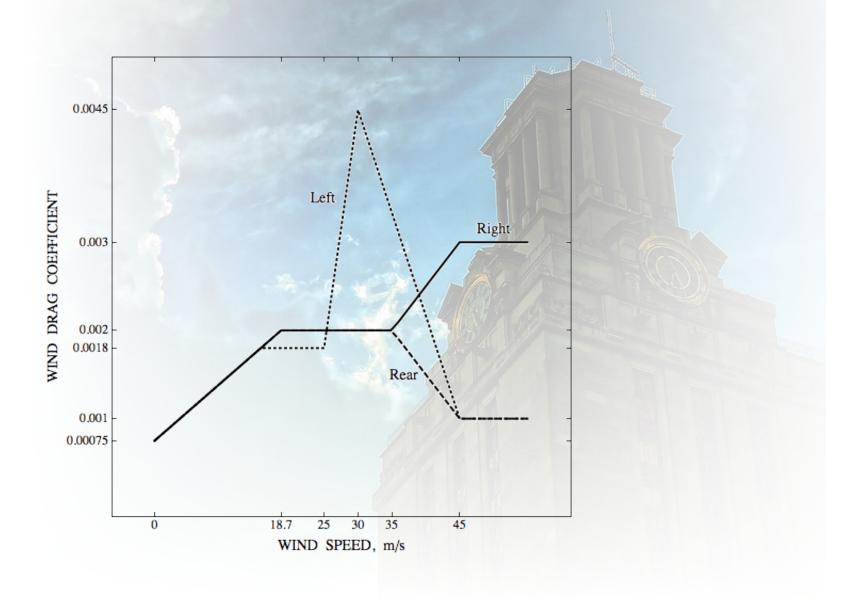
with similar expressions for the wind drag coefficient:

$$C_d = \frac{1}{1000} \left( \frac{15}{20} + \frac{40}{600} U_{10} \right)$$
 ADCIRC (Garratt, 1977)

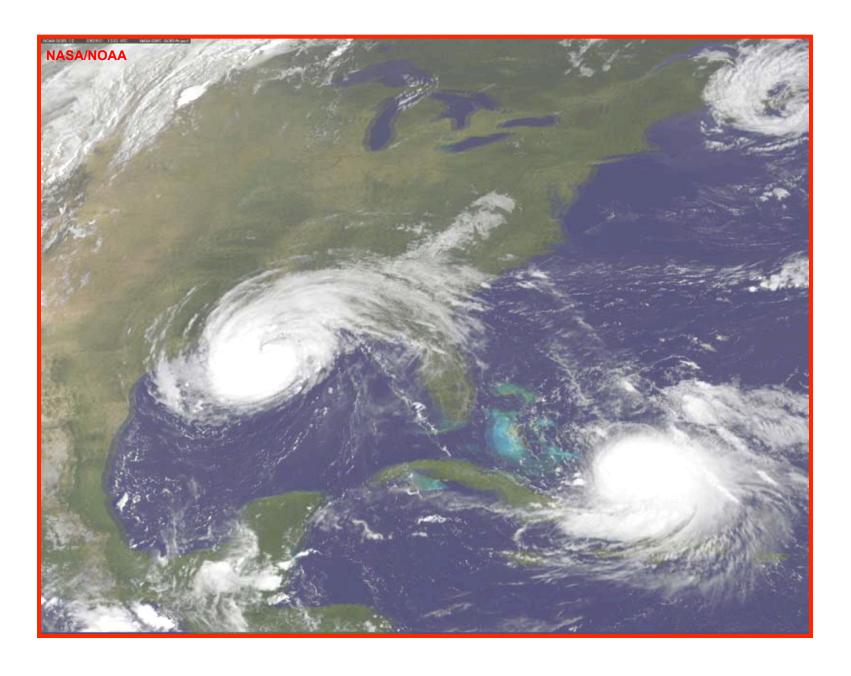
$$C_d = \frac{1}{1000} \left( \frac{16}{20} + \frac{39}{600} U_{10} \right)$$
 SWAN (Wu, 1982)

with an upper limit of  $C_d \le 0.002$ .

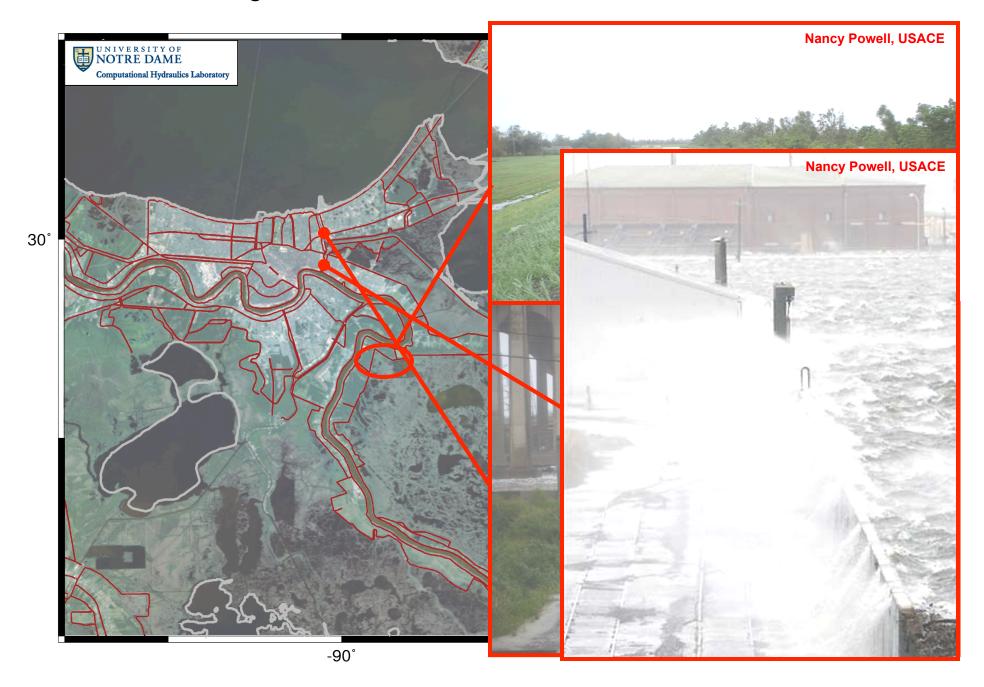
# **Coupled Physics** STORM LEFT **RIGHT** WINDS WIND WAVES **SWELL REAR**



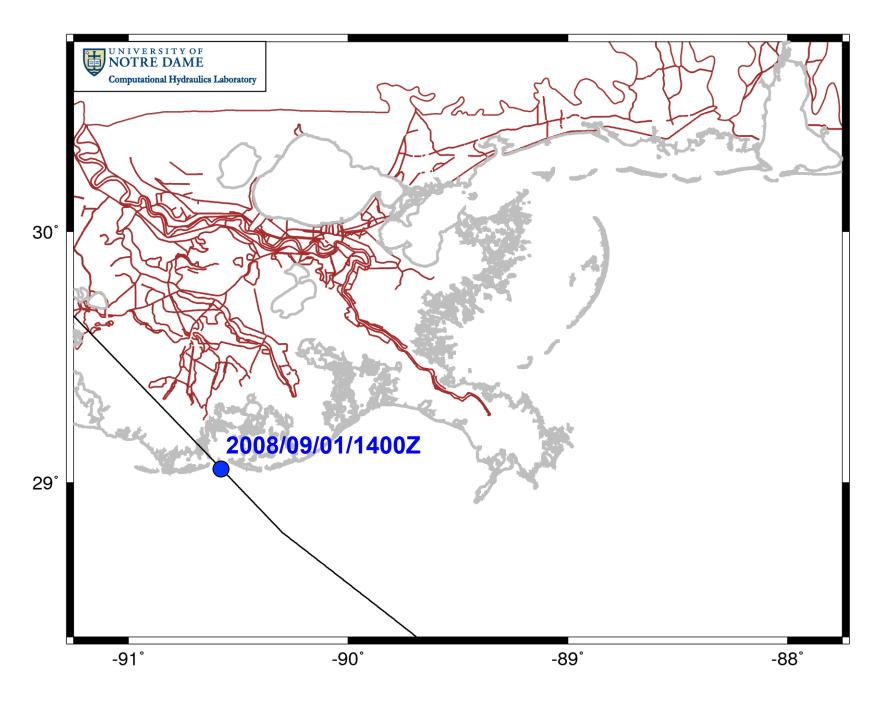
# Hurricane Season 2008



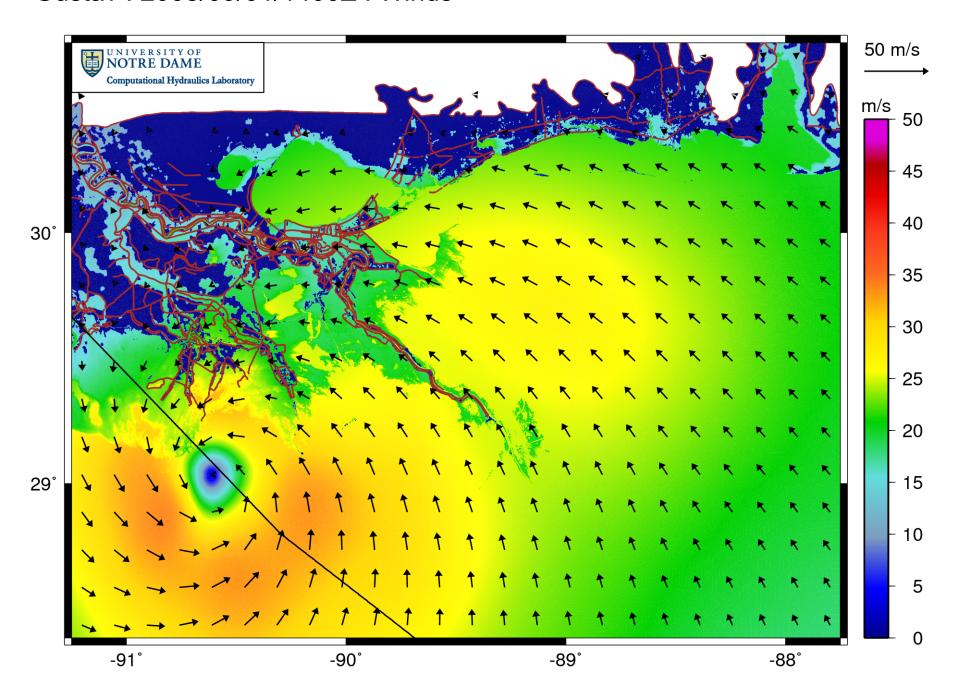
# Gustav: Storm Surge near New Orleans



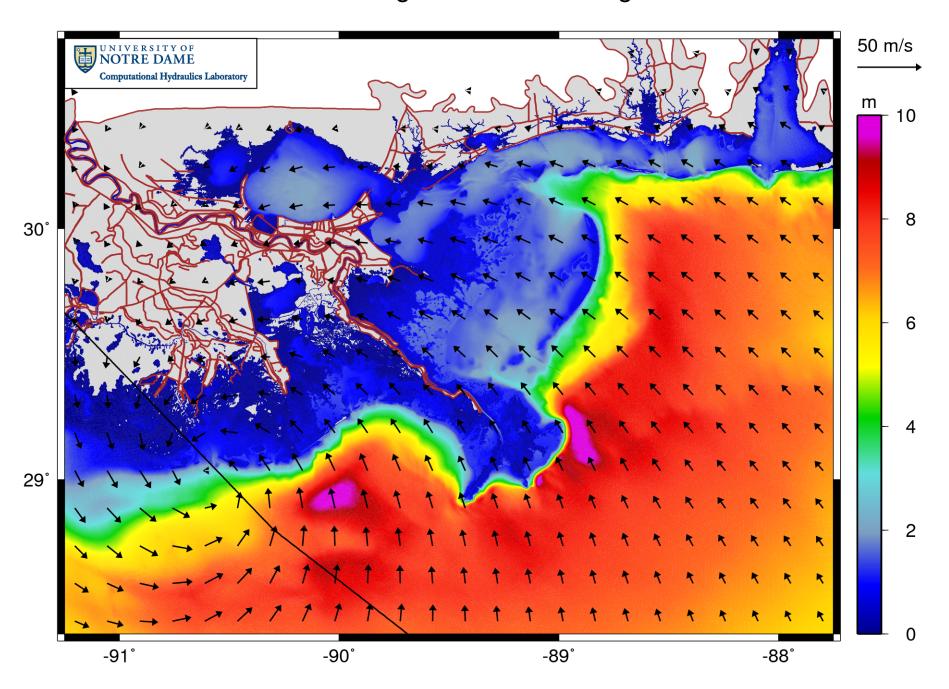
# Gustav: Track



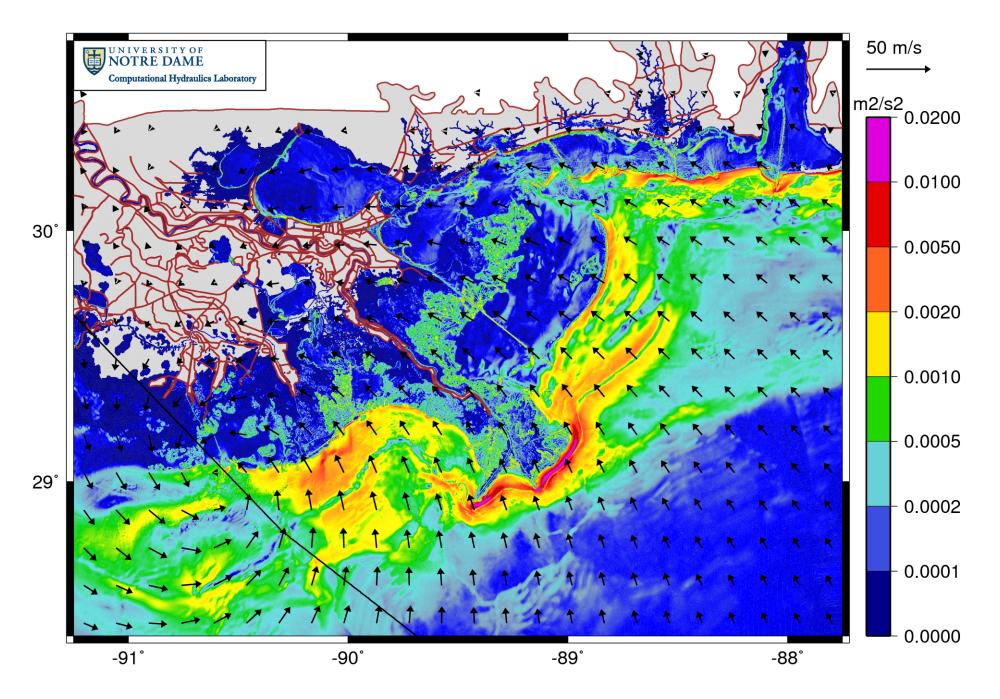
#### Gustav: 2008/09/01/1400Z: Winds



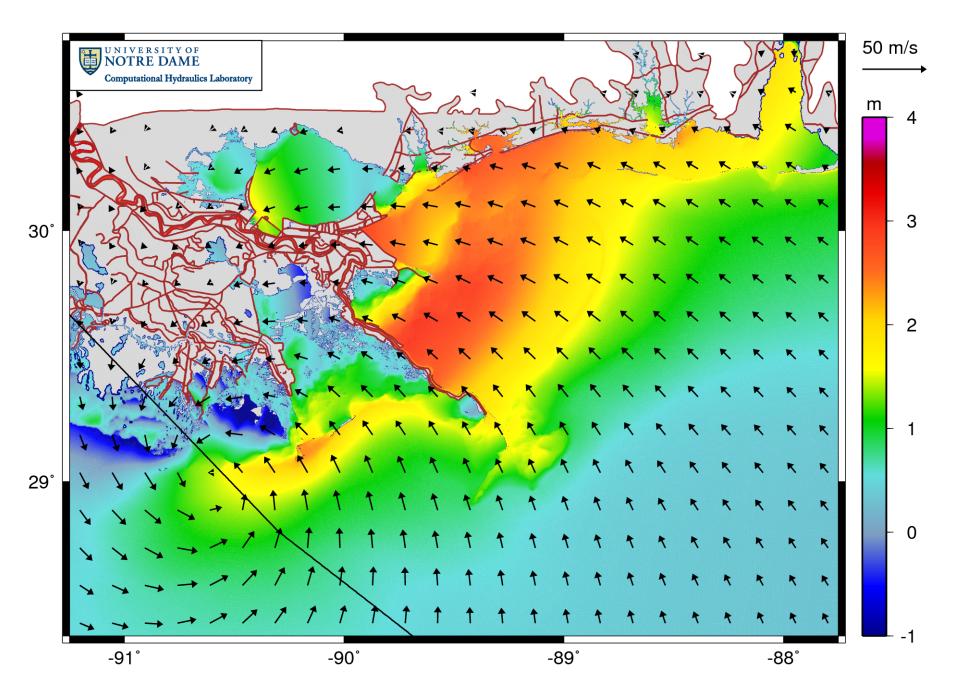
# Gustav: 2008/09/01/1400Z: Significant Wave Heights



#### Gustav: 2008/09/01/1400Z: Radiation Stress Gradients



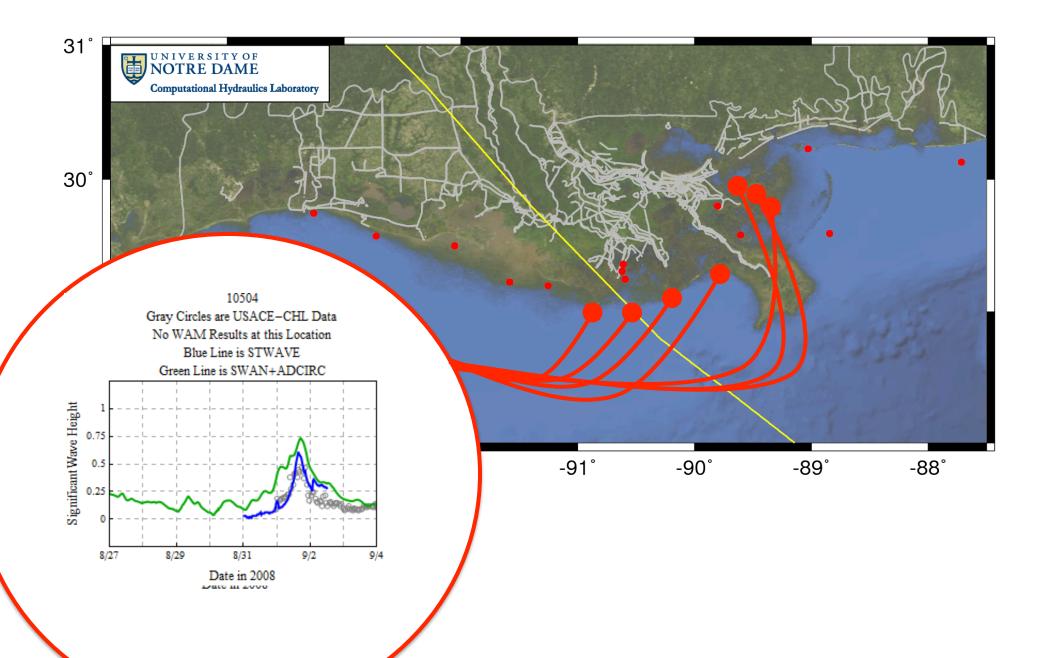
## Gustav: 2008/09/01/1400Z: Water Levels



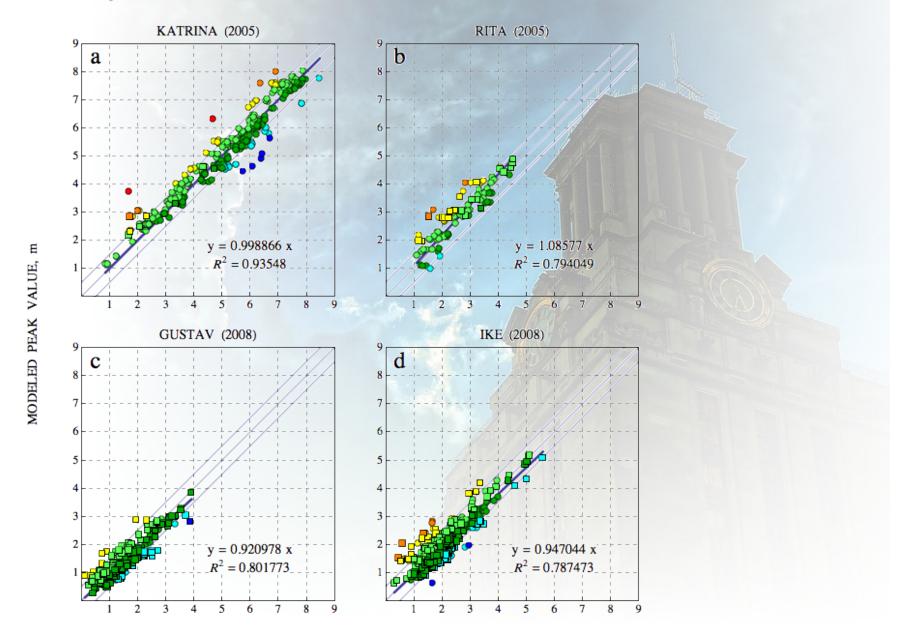
# Increased Availability of Measurement Data

	Katrina (2005)		Gustav (2008)	
High-Water Marks	Total:	399	Total:	82
	URS/FEMA	193	URS/FEMA	82
	USACE	206		
Time Series	Water Levels:	9	Water Levels:	443
			CSI	5
			Andrew Kennedy	16
	NOAA	3	NOAA	26
			USACE-CHL	6
			USACE	54
		37/6	USGS (Deployable)	61
	USGS (Permanent)	6	USGS (Permanent)	48
			CRMS	243
	Wave Parameters:	17	Wave Parameters:	39
	NDBC	14	NDBC	12
	CSI	3	CSI	5
			Andrew Kennedy	16
			USACE-CHL	6

# Gustav: Validation: Significant Wave Heights



# Validation: High-Water Marks



#### Conclusions and Future Work

## 'Loose' Coupling of Waves and Surge:

- Successful hindcasts of Katrina and Rita
- WAM and STWAVE were clunky but effective

## 'Tight' Coupling of SWAN+ADCIRC:

- Models use same unstructured mesh; Information passed dynamically
- SWAN is as accurate as WAM and STWAVE
- Coupled model is efficient to 1000s of computational cores

#### **SWAN+ADCIRC Hindcast of Gustav:**

- Next generation of meshes in Louisiana and Texas
- Wealth of measurement data, including nearshore waves

## Couple SWAN with ADCIRC(DG):

Preliminary work is promising